Aftertreatment System Durability for Future Low NO_X Engines

SOUTHWEST RESEARCH INSTITUTE®

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Agenda

- Defining Durability versus Robustness
- Regulatory Requirements
- Durability Challenges and System Demands
- Low NO_X Durability Example (CARB Stage 3 Engine)
- Assessing Aftertreatment Durability
 - -Accelerated Aging Methodology (DAAAC)
- Facilities for Accelerated Aging
- Summary and Conclusions

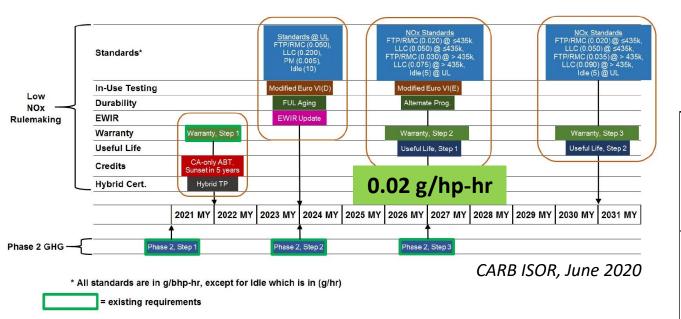


Definitions

- Durability and Robustness are not the same thing
 - Proper system design can improve both
- Durability describes the resistance of a system to "normal" modes of degradation
 - A system can degrade and still be within normal operating limits
 - Normal degradation is expected we can design for this
 - Proper design for good durability means understanding field operations and conditions
 - Durability can be helped by feedback controls and long-term trim functions
- <u>Robustness</u> describes the resistance of a system to "abnormal" modes of degradation
 - Generally associated with a system failure
 - Abnormal degradation is not expected we cannot easily predict failures
 - Proper design for robustness means understanding potential system failure modes (FMEA)
 - Diagnostics are the primary defense against failure in use spot failures and limit the damage



Requirements - Simultaneous NO_X and CO₂ Reduction



- Meeting Upcoming Regulatory Targets will Require Simultaneous Reductions on NO_X and CO₂
- This will increase the requirement for Aftertreatment performance and durability

		FTP				
		14%	86%			
		Cold	Hot	SET	LLC	
		g/hp-hr	g/hp-hr	g/hp-hr	g/hp-hr	
	Standard	0.020		0.020	0.050	
Certification Targets	Engine-Out	2.8	3.1	4.0	3.0	
	Conversion	99.2%	99.8%	99.8%	99.4%	
	Tailpipe	0.022	0.006	0.008	0.018	
	TP Composite		0.009			
	EO Composite		3.1			
	Composite Conversion		99.8%			
L Compliance	FUL Conversion	98.7%	99.6%	99.6%	98.7%	
	FUL Tailpipe	0.038	0.012	0.016	0.039	
	FUL Composite Conversion		99.5%			
	IRAF		0.002	0.002	0.006	
	Final TP Composite		0.017	0.018	0.045	
FUL	FUL Durability Loss Margin		0.3%	0.2%	0.7%	

- Aftertreatment Conversion Efficiency Demand is > 99.5% at end-of-life
- Margin for Loss of Conversion ~ 0.25% (0.7% at low load)

Requirements - Increased Full Useful Life Periods

CARB Increased FUL Requirements from Low NO_x Rule

	Useful Life		Warranty			
Category	Step 1	Step 2	Step 1	Step 2	Step 3	
	2027	2031	2022	2027	2031	
HHD Diesel	600,000 mi	800,000 mi	350,000 mi	450,000 mi	600,000 mi	
> 33,000 [bs	11 years, 30,000 <u>hrs</u>	12 years, 40,000 <u>hrs</u>	5 years	7 years, 22,000 <u>hrs</u>	10 years, 30,000 <u>hrs</u>	
MHD Diesel > 19,500 lbs <= 33,000 lbs	270,000 mi 12 years	350,000 mi 15 years	150,000 mi ^{5 years}	220,000 mi 7 years, 11,000 <u>hrs</u>	280,000 mi 10 years, 14,000 <u>hrs</u>	
LHD Diesel > 14,000 [bs <= 19,500 [bs	190,000 mi ^{12 years}	270,000 mi ^{15 years}	110,000 mi 5 years	150,000 mi 7 years, 7,000 <u>hrs</u>	210,000 mi 10 years, 10,000 <u>hrs</u>	
HD Otto	155,000 mi	200,000 mi	n/a¹	110,000 mi	160,000 mi	
> 14,000 [bs	12 years	15 years		7 years, 6,000 <u>hrs</u>	10 years, 8,000 <u>hrs</u>	

¹ No Step 1 change, current HDOE warranty is 50,000 miles, 5 years

- Current Diesel FUL: HHD = 435,000 MHD = 185,000 LHD = 110,000
- Current Otto FUL = 110,000 miles

- CARB Low NO_X Omnibus extended FUL ~ X2
- EPA is also examining extending FUL requirements
- More stringent in-use requirements also increases demand for real Aftertreatment durability

Class 8 Durability Increase from 700000 km to 1290000 km by 2031

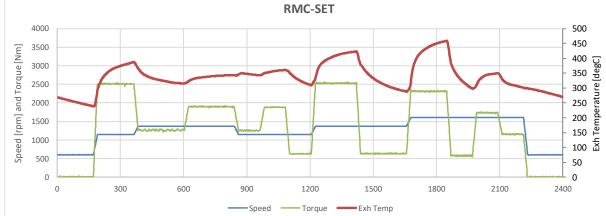


SCR Durability Challenges



Low Load





- Low Temperature Conversion on intermittent high load transients
- Durability challenge = maintain Low T Conversion
 - Chemical poisons
 - Sulfur management
 - Maintain DOC NO-NO₂ feed-gas performance
 - High T exposure impact on storage



- Very High Conversion at High Flow and NO_X Rates
- Durability Challenge = maintain high T selectivity of NH₃ oxidation
 - High Temperature Durability
 - Slip Catalyst Selectivity
- Manage storage capacity changes to prevent excessive slip

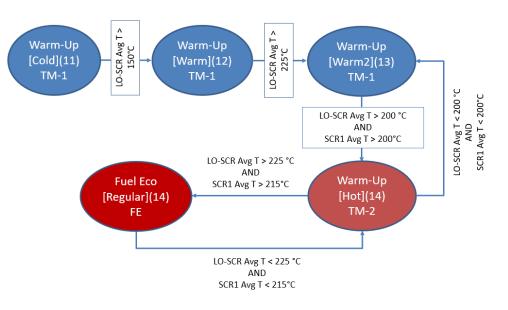
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Other Key System Elements for Aftertreatment Durability at Low NO_X

- Very good DEF evaporation and mixing
 - especially for high load, high NO_X conditions with high DEF demand
- Sensors and Actuators
 - accurate sensors that are stable over time (NO_X and NH₃)
 - repeatable and reliable DEF and HC dosing
- Good regeneration controls
 - Periodic regenerations and $deSO_X$ events will be needed
 - Preventing excessive localized temperatures is critical to maintain Aftertreatment
 Durability

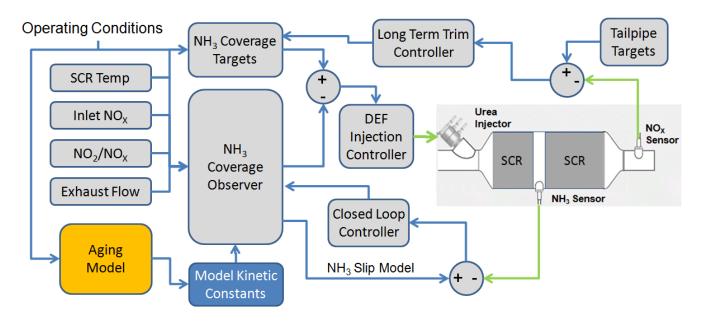


The Role of Controls in Aftertreatment Durability



Engine – Thermal Management

Aftertreatment – Model Based DEF Dosing Controls



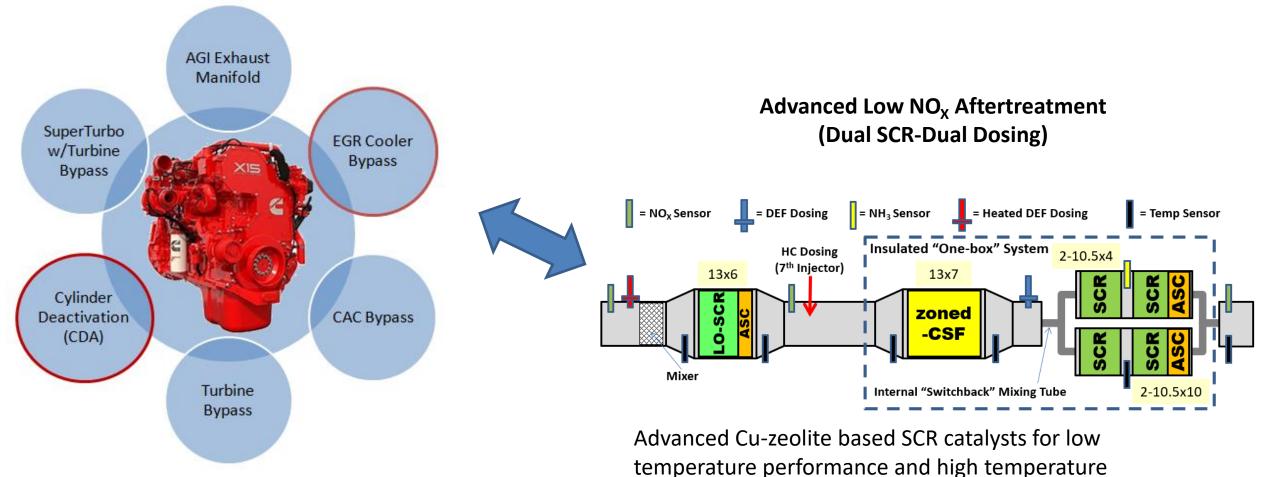
- Better thermal management control results in higher system temperatures
- Aftertreatment less affected by low temperature conversion losses due to chemical poisoning

- Model-based controls for improved flexibility
- High Speed Feedback too maintain precision at high NO_X conversion (> 99.5%)
- Long-term trim to compensate for model-input errors
- Catalyst aging model



Stage 3 Low NO_X Engine Example

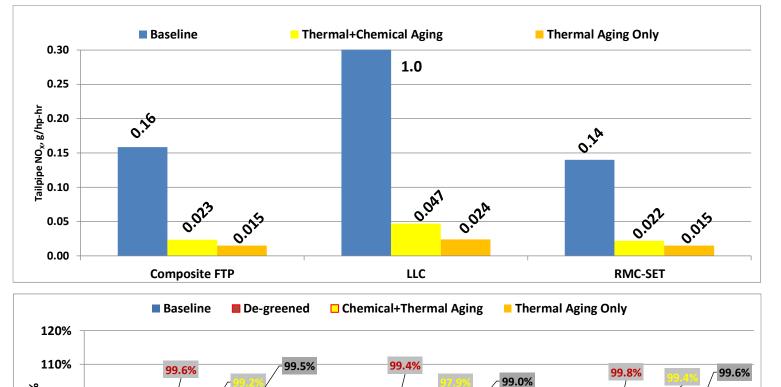
2017 Cummins X15 Engine with Eaton CDA Hardware



durability

SwRI

Stage 3 Demonstration System Durability



65%

LLC

- Values shown as tested
 - 0.002 added to FTP/RMC for IRAF (regeneration adjustment, "k-factor")
 - 0.006 added to LLC for IRAF
- Margin available to standard as calibrated = 0.2% for FTP/RMC and 0.7% for LLC
- Degradation with Full Aging (Thermal + Chemical) $\sim 0.4\%$ for FTP/RMC and 1.5% for LLC
- <u>Thermal aging only not sufficient,</u> especially at lower temperatures



94%

Composite FTP

%

Š

%100% 800, %

80%

70%

60%

95%

RMC-SET

Stage 3 System - Opportunities for Further Improvement in Durability of NO_X Performance

- Move to traditional DOC + DPF architecture
 - Better long-term NO-NO₂ oxidation (downstream SCR feedgas)
 - More robust and likely slightly better CO_2
- Further improvement in downstream mixing
- Small Increase in downstream catalyst volume for high load points
- Catalyst Formulation
 - More low temperature chemical poisoning resistance
 - Better long-term high temperature selectivity of NH_3 oxidation
- Further Controls Improvement Catalyst Aging Model
- Target = Reduce Aging Impact by Half

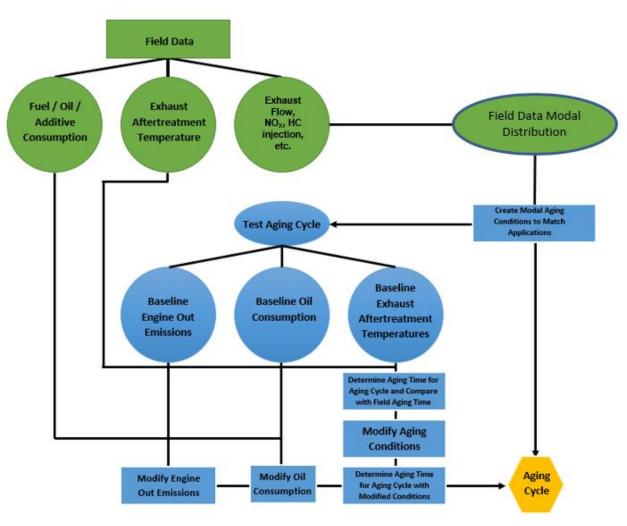


Assessing Aftertreatment Durability

- Laboratory Assessment of Durability is Important for Multiple Reasons
 - Certification pre commerce demonstration of system design (Due Diligence)
 - Development aged parts are needed to understand necessary design margins
- Traditional Approaches
 - Normal Engine Aging
 - Full Useful Life very time consuming (10000 hours FUL for heavy-duty on-road)
 - Partial Life still time consuming and requires extrapolation which has been shown to be inaccurate
 - These issues will get worse with increased FUL (20000 hours FUL for heavy-duty on-road)
 - Hydrothermal Aging (Oven)
 - Not representative of real-world aging
 - \bullet Does not accurately capture key mechanisms for Low $NO_{\!X}$
- Accelerated aging methodology that captures all aspects of aging



DAAAC (Diesel Aftertreatment Accelerate Aging Cycles) Protocol

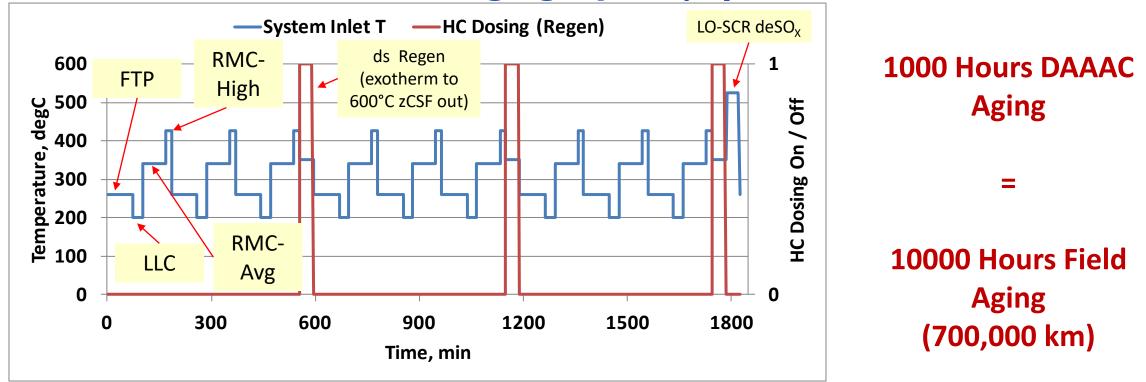


- DAAAC Protocol is a method of generating representative, accelerated aging cycles based on field data
 - Not one specific cycle
 - Target is IOX acceleration
 - Aftertreatment-centric approach
- Thermal, Chemical, and Physical Aging Incorporated
- Conditions relevant to field
 - Aging temperatures are not beyond normal field maximums
 - Regenerations conducted in similar fashion to real application
 - Representative normal oil formulations



Stage 3 Low NO_X Demonstration

DAAAC-Based Accelerated Aging Cycle (equivalent to 300 field hours)



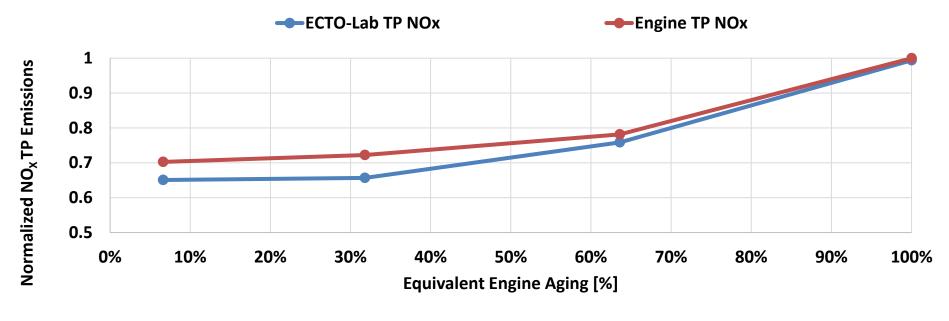
- Regeneration 30 min every 100 hours at 600°C zCSF Outlet Temperature
 - Regeneration using actual exotherm via 7th injection fuel injection in front of zCSF
- LO-SCR long-term deSO_X 30 min every 300 hours at 525°C LO-SCR Inlet T (later modified to 550°C)
- Oil exposure at I0X (combination of modified engine and fuel doping)
- Sulfur exposure at I0X (extra sulfur doped in fuel ~ 2.5ppm SO₂ in exhaust)
- Chemical exposure 138 kg oil, 183 g/L sulfur on LO-SCR peak filter ash load 35 g/L reached every 500 hours POWERTRAIN ENGINEERING



ECTO-Lab (Burner) Aging Using DAAAC

Correlation with Engine-Based Deterioration Factor

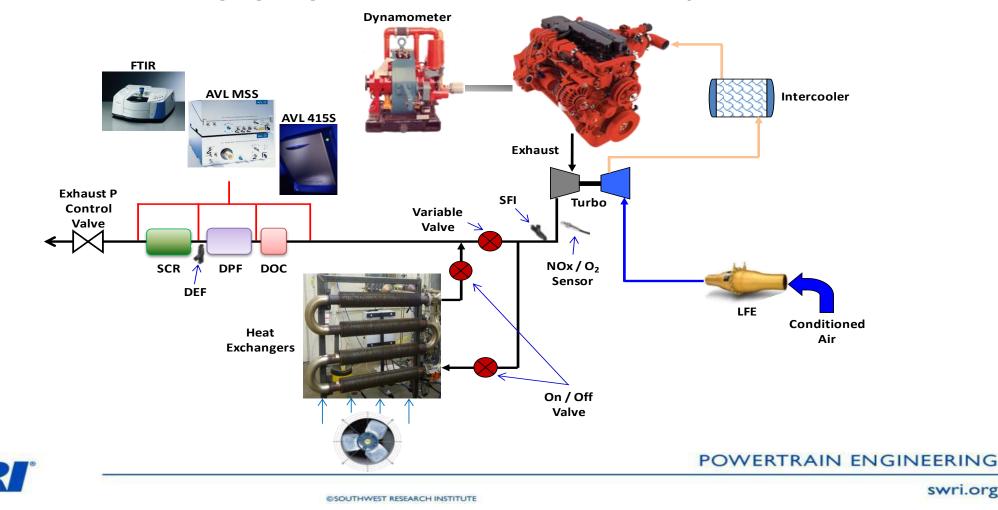
- As Shown Below, the End Result is an ECTO-Lab Aged System That Successfully Replicates the Performance of the Engine Aged System
 - With Oil and Sulfur Exposure
 - But DAAAC was conducted in 1 / 10^{th} the amount of time
- The ECTO-Lab Aged System is Within 1% of the Engine Aged System



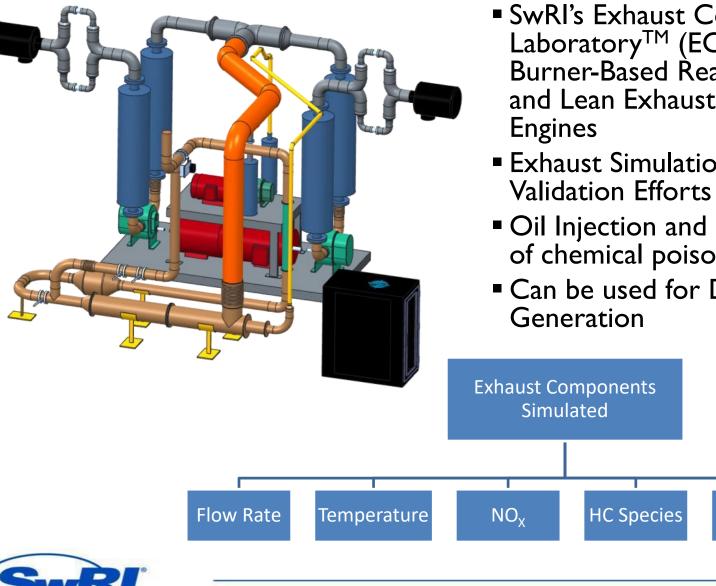


SwRI Engine-Based DAAAC Platform

- Highly flexible engine bench used to evaluate age and evaluate diesel aftertreatment components and sensors
- DAAAC modified bench aging engine for increased oil consumption



SwRI Burner-Based DAAAC Platform - ECTO-LabTM



- SwRI's Exhaust Composition Transient Operation LaboratoryTM (ECTO-LabTM) is a Computer Controlled, Burner-Based Reactor Used to Replicate Stoichiometric and Lean Exhaust Conditions of Conventional SI and CI Engines
- Exhaust Simulation Capabilities Enables Calibration and Validation Efforts on Full-Size Components
- Oil Injection and SO₂ injection for DAAAC acceleration of chemical poisoning (I0X)

 $H_{2}O$

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Can be used for DAAAC Aging and OBD Part Generation

 O_2

Summary and Conclusions

- Aftertreatment Durability is Critical for meeting Future Low NO_X Standards
 - New Standard are Increasing Demand for Durable High NO_X Conversion > 99.5%
- Aftertreatment Durability Requires a Systems Approach
 - Catalyst Formulation
 - Aftertreatment Design
 - Engine Calibration
 - Controls
- Stage 3 Demonstration Indicates Potential but More Work Needed on Aftertreatment Durability to Insure Sufficient Margins
- New Approaches to Accelerated Aging of Diesel Aftertreatment are Needed to Properly Assess Durability
 - SwRI DAAAC Protocol Meets this Need
 - Specialized Facilities for DAAAC Accelerated Aging are Available



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